

The density of liquids used in certain industrial processes is important information to assure the quality of the end product. Let us for example consider mouthwash. Particular mouthwashes consists of water, glycerin and alcohel in specific amount. Mixing them by volume might lead to improper mixing since, for instance, water might already have been absorbed by the alcohol and glycerin prior to the mixing. Measurement of the liquids' density along with volumetric flow or simply mass flow resolves the issue. Additionally to minimize the total uncertainty in the process, a balance check can be performed subsequently to mixing using mass flow information [1]. Measuring the mass flow or the combination of volumetric flow and density of the flowing liquids is hence important to some industrial applications.

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There are several mater types capable of estimating mass flow, each with its own advantages and weaknessess. One type is an ultrasonic mass flow meter which combines a standard ultrasonic flow meter and an ultrasonic densitionneter [2]. The ultrasonic densitionneter can be incorporated into one of the flow meter's transducers, than to adding any additional transducers. Although one can find patents for ultrasonic mass flow meter dating from the 1950's, they are not a production item. Several issues have afflicted the ultrasonic densitionneters. This paper presents the theory behind the pulse each outlasonic densitionneter and follows with its drawbacks. The published solutions to some of those drawbacks are discussed. The foulting issue is presented and a solution introduced. A simulation setup reveals the problem and supports the proposed solution. The concept behind the pulse-each outlrasonic densitioneter relies on the reflection of sound from the interface that joins the probe and the liquid. The coefficient of reflection R is the

ratio of the amplitude of the reflected wave $A_{\rm r}$ at the interface to the amplitude of incident wave $A_{\rm t}$ such that $R=A_r/A_t$. $R_{\rm t}$ for normally incident ultrasonic pulse, is also

(1)

An $z_p + s_l$ (1) where z_p are the characteristic acoustic impedance of the probe and liquid respectively [3]. The acoustic impedance of the probe and liquid respectively [3]. The acoustic impedance for progressive plane waves is defined as the product ρ with ρ being the density of the medium and e the speed of sound through the medium. This model is for continuous waves but has been used in pulse-either techniques [4-7]. If A_l and z_p are previously known while A_l , is measured then the acoustic impedance of the liquid z_l can be calculated. The density of the liquid ρ_l is simply u/c_l , e_l , the speed of sound in the liquid, is obtained by placing a reflector within the liquid at a known distance d_l . The part of the pulse transmitted into the liquid reflects back from the reflector and e_l is the ratio 2d to the time separating the true cahoes. Fig. I shows an illustration of this stupy with its lattice diagram and the received signal.

Beyond this simple idea, there are issues that have slowed the introduction of the ultrasonic densitioneter into the field. The amplitude of the emitted pulse A_l can vary, influencing directly the amplitude of the echo A_r . This can occur with a

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I. INTRODUCTION The density of liquids used in certain industrial processes is important information to product. Let us for example consider mouthwashes consist of water, glycerin and alcohol Detrotorifut, and controllisting the error inchicing thin by the teleplotits on an improper mixing since, for insultrasonic densitometer for liquide nave been absorbed by the alcohol enghaly cerito minimal presentations. Measurement of the liquids' density along With mixel and a tries of the World of the liquids' density along with mixel and the liquids' developed and the liquid and the li resolves the issue. Additionally to minimize the total uncertainty in the process, ###alance with the performed sub quently to mixing from the density and the first property throughout of the typical of the figure of the first property throughout of the typical of the first property through the first property through the first property through the first property through the first through the figure of the first density, also known as found through the figure of the first density, also known as found to the first property through the first property throug ss flow or the combination in the property of the flowing liquids is hence N'A important straightful and the straightful and I. INTRODUCTION The density of liquids used in certain industrial processes is The density of liquids used in certain industrial processes is important information to assure the quality of the end product. Let us for example consider mouthwash. Particular mouthwashes consists of water, glycerin and alcohol in specific amount. Mixing them by volume might lead to improper mixing since, for instance, water might already have been absorbed by the alcohol and glycerin prior to the mixing. Measurement of the liquids' density along with volumetric flow or simply mass flow resolves the issue. Additionally to minimize the total uncertainty in the process, a balance check can be performed subsequently to mixing using mass flow information [1]. Measuring the mass flow or the combination of volumetric flow and density of the flowing liquids is hence important to some industrial applications. ratio of the amplitude of the reflected wave A_τ at the to the amplitude of incident wave A_τ such that R=A for normally incident ultrasonic pulse, is also $\begin{aligned} z_p + z_i \\ \end{aligned}$ where z_p and z_i are the characteristic acoustic impedance of the probe and liquid respectively [3]. The acoustic impedance for progressive plane waves is defined as the product c_i with p being the density of the medium and c_i the speed of sound through the medium. This model is for continuous waves but has been used in pulsa-cebe tochariques [4–7]. If A_i and z_j are previously known while A_i is measured then the acoustic impedance of the liquid z_i can be calculated. The density of the liquid z_i and z_i is obtained by placing a reflector within the liquid at s_i known distance d_i . The part of the pulse transmitted into the liquid reflects back from the reflector and a_i is the ratio $2d_i$ to the time separating the two achoes. Fig. 3 shows an illustration of this secup with its lattice diagram and the received signal. Beyond this simple idea, there are issues that have slowed the introduction of the ultrascenic densitometer into the field. The amplitude of the entitled pulse A_i can vary, influencing some industrial applications. There are several meter types capable of estimating mass flowing cach with its own advantages and weaknesses. Once type is an ultrasonic mass flow meter which combines a standard trasonic flow meter and an ultrasonic densitometer [2]. The ulinstitution of the control of the co **IEEE Personal Acc** d Help? Follow CHANGE USERNAME/PAS The amplitude of the emitted pulse A_i can vary, influencing directly the amplitude of the echo A_o . This can occur with a CANADA: +1 800 678 4333 f in .DWIDE: +1 732 981 0060 ACT & SUPPORT 0-7803-7705-2/03/\$17.00 ©2003 IEEE About IEEE Xplore | Conta A not-for-profit organization, IEEE is the world's largest technical professional organization dedicated to advalHide First:Page Preview efit of humanity.

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